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PIANO NAZIONALE DI RIPRESA E RESILIENZA



NQSTI
National Quantum Science
and Technology Institute

Kinetic Inductance Traveling Wave Parametric Amplifiers for Practical Microwave Readout

Andrea Giachero

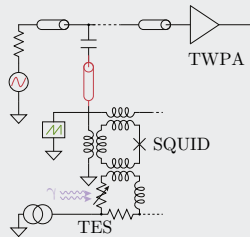
University of Milano-Bicocca

INFN - Milano-Bicocca

Bicocca Quantum Technologies (BiQuTe) Centre



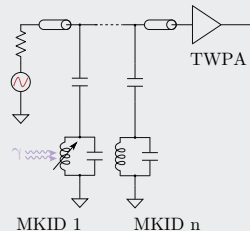
TES and MMC detectors



rf-SQUID multiplexing of TES/MMC microcalorimeter arrays for x-ray and gamma-ray spectroscopy.

Appl. Phys. Lett. 122, 214001 (2023)

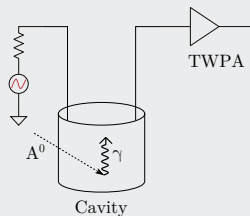
MKIDs detectors



Optical or Phonon-Mediated MKIDs are naturally frequency domain multiplexed detectors

Appl. Phys. Lett. 115, 042601 (2019)
arXiv:2402.05419 [physics.ins-det]

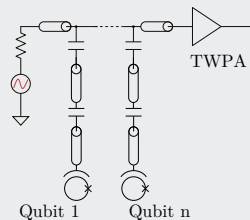
Resonant microwave cavity



Resonant cavity haloscope readout to perform broadband axion searches

Rev. Sci. Instrum. 94, 044703 (2023)
Phys. Rev. D 108, 062005

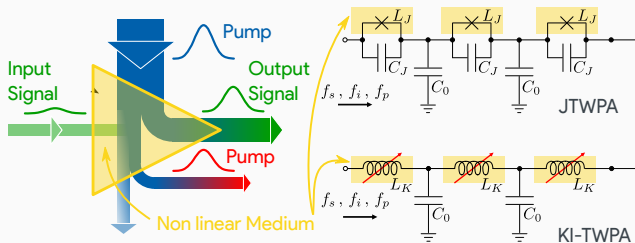
Quantum bit



Fast and high-fidelity readout of simultaneous superconducting qubits

Appl. Phys. Lett. 113, 242602 (2018)
Phys. Rev. Applied 10, 034040 (2018)

- TWPA: non linear transmission line;
- The nonlinear element can be implemented by Josephson Junction (JJ) or Kinetic Inductance (KI) of superconductors;
- A large pump tone modulates this element, coupling the pump (f_p) to a signal (f_s) and idler (f_i) tones via frequency mixing;

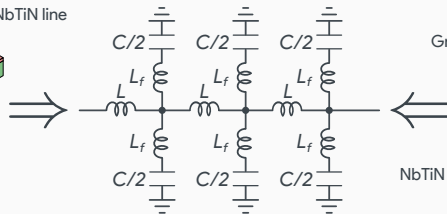
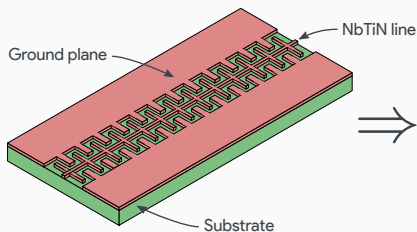


JTWPA's have become important for superconducting-circuit experiments such as multiplexed qubit readouts and sensing.

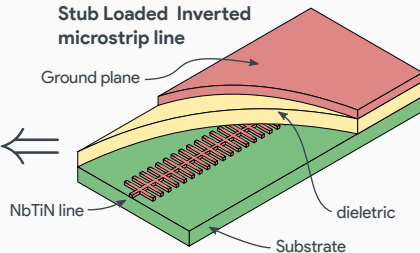
... however, the development of Kinetic Inductance TWPA (KI-TWPA or KIT) is particularly significant because they

- are **simple to fabricate** and require only few lithography and etching steps, without overlapping structures;
- provide a **high dynamic range, high gain, and operate near the SQL**;
- can **operated also at higher temperatures**, from millikelvin to 4 K (space application, spin-qubit, ...);
- are **resilient to high magnetic fields** (spin-qubit, axion search, ...);

Stub loaded CPW line



Stub Loaded Inverted microstrip line



Stub-loaded CPW:

- Originally proposed by NIST in 2017;
- Capacitance (C) due to the stub length and to the gap between the ground plane and the central line:
 \Rightarrow Ideal for modest kinetic inductance values ($L_k \sim 10$ pH/sq);
- The central line and ground plane are very close ($\sim 1 \mu\text{m}$)
 \Rightarrow High probability of a short to ground
 \Rightarrow Very low fabrication yield (10%);

Stub-loaded IMS:

- Capacitance (C) due to the stub-length, to the dielectric permittivity and thickness:
 \Rightarrow More degree of freedom having a C to match a high L
 \Rightarrow Ideal for high kinetic inductance values ($L_k > 30$ pH/sq);
- Shorter elementary cell \Rightarrow compact design;
- Ground plane and central line are totally isolated
 \Rightarrow Very low fabrication yield (>90%);
- Dielectric could introduce losses;

KI-TWPA based on 20 nm thick NbTiN film have shown promising noise performances \Rightarrow near-quantum-limited amplifier

- Series of coplanar waveguide (CPW) sections (cells) with inductance \mathcal{L} and capacitance to ground \mathcal{C} tuned by the finger length: $Z_0 = \sqrt{\mathcal{L}/\mathcal{C}}$
- Super-cell composed by $N_u = 60$ with $Z_0 = 50 \Omega$ and $N_l = 6$ with $Z_0 = 80 \Omega$ to create a weakly dispersive line.
- Good performance at 30 mK

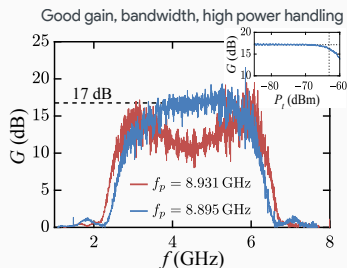
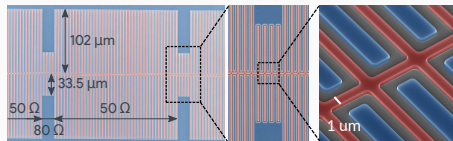
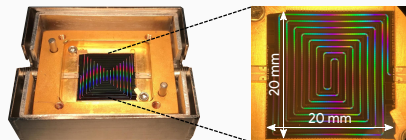
M. Malnou et al. PRX Quantum 2, 010302 (2021)

- Good performance at 4 K
- Readout demonstration with rf-SQUID and TESs

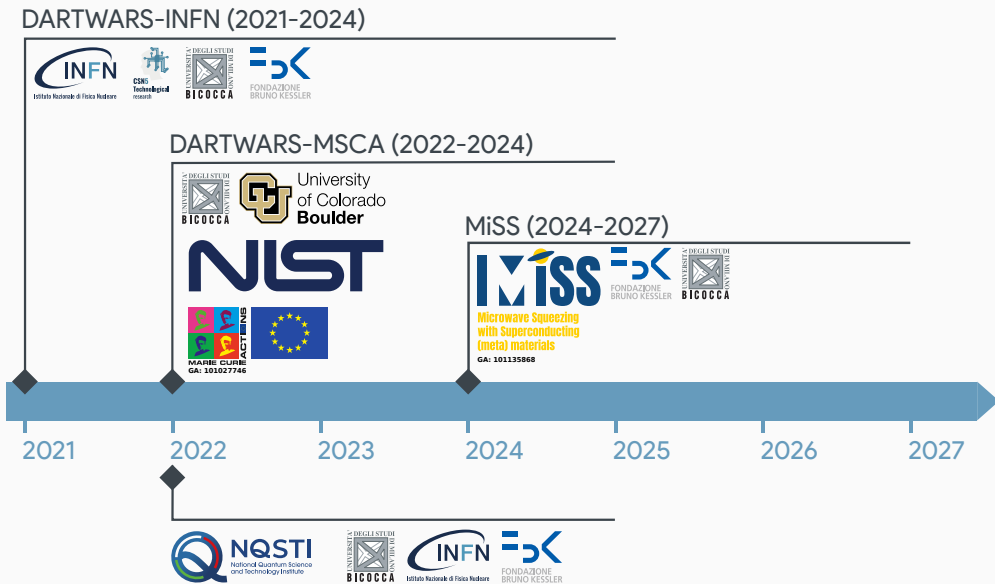
M. Malnou et al. Appl. Phys. Lett. 122, 214001 (2023)

... but...

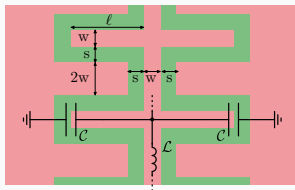
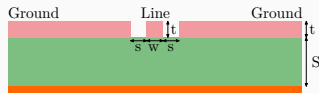
- very high pump power to operate;
- very low fabrication yield (<10%);



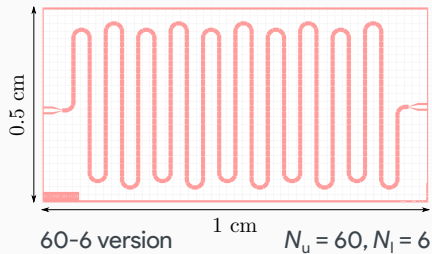
Material: NbTiN
 Thickness: 20 nm
 L_k : 10 pH/sq
 T_c : 15 K
 Gain: 17 dB
 Bandwidth: 3.5–5.5 GHz
 Noise: 3.1 quanta
 Pump Power: -28 dBm
 I_{dc} : 1.5 mA
 I_* : 7 mA



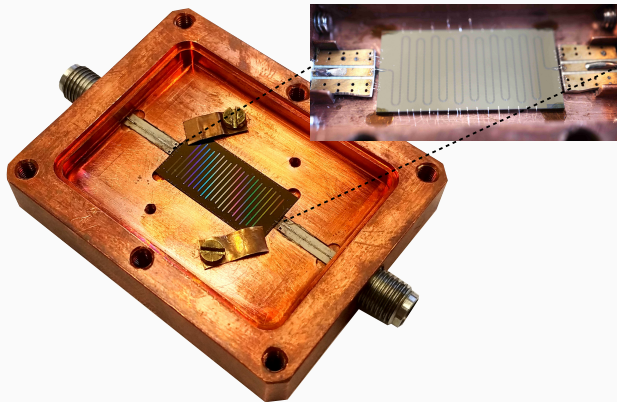
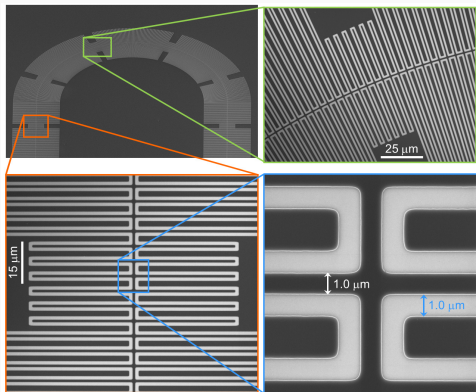
Si-substrate NbTiN Copper Box



- NbTiN line with kinetic inductance $L_k = 8.5$ pH/sq produced in collaboration with FBK;
- Conservative stub-loaded CPW line (inspired by PRX Quantum 2 (2021) 010302)



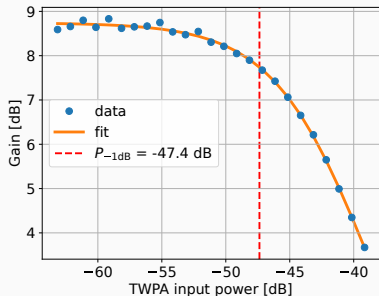
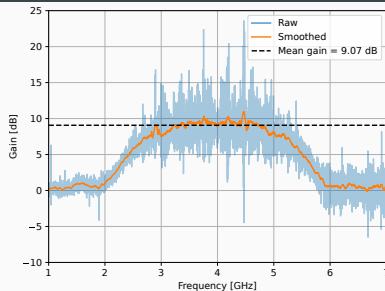
- Meander-shaped line to simplify the design
- Each supercell composed by:
 - $N_u = 60$ unloaded cells and $N_l = 6$ loaded cells;
- Total number of supercells: $N_{sc} = 523 \Rightarrow$ *half-size*;
- Total number of cells: $N_c = 34518 \Rightarrow$ Total line length: $L_{tot} \sim 17.3$ cm;
- Chip sizes: 0.5×1 cm²;
- Expected gain: $G \sim 10$ dB, centered at 6 GHz;
- Expected pump frequency: $f_p \sim 12$ GHz;



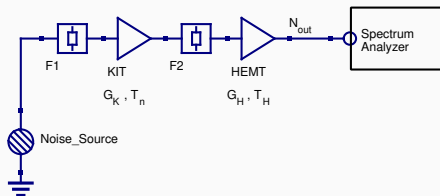
Design, production and characterization published in:

- *Phys. Scripta* 98 (2023) 12, 125921
- *IEEE Trans. Appl. Supercond.* 34,3 (2024) 1700605
- *J. Low Temp.Phys.* 216 (2024) 1-2, 156-164

- Amplification bandwidth centered around 4 GHz (lower than expected);
- Maximum gain measured around 9 dB in the 3 dB bandwidth, which aligns with the expected value;
- Critical current of $I_c = (1.41 \pm 0.01)$ mA and a scaling current of $I^* = (6.72 \pm 0.03)$ mA, as expected and compatible with literature;
- 1 dB compression point estimated at $P_{-1dB} = -47.4$ dB;
- Higher pump power yields higher gain, but it also introduces larger ripples in the gain curve:
⇒ not optimized box, local heating on the chip (hot-spots)
not optimized grounding, etc
- Very encouraging performances for this first prototypes production



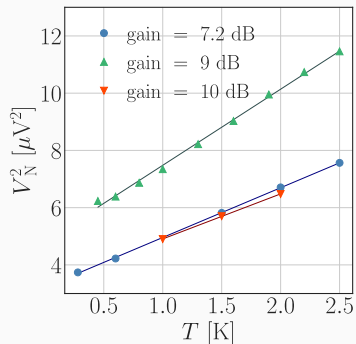
- Measurement of noise using the Y-factor method \Rightarrow Johnson-Nyquist noise of a 50Ω resistor at various known temperatures;
- Noise source with an adjustable temperature range between 0.28 and 2.5 Kelvin.
- Noise measurements at three different gain settings: 7 dB, 9.2 dB, and 10 dB;
- Previous calibration of all system attenuation (including the line and RF components) and gains (HEMT and warm amplifiers) during dedicated cooling cycles.



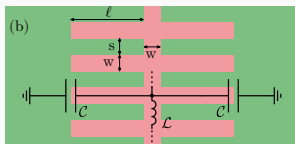
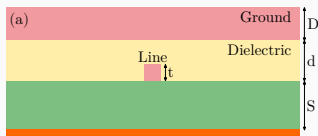
Noise measurements results @ 4 GHz			
G_K (dB)	7.2	9.0	10
T_{sys} (K)	1.78	1.72	2.06
T_n (K)	0.5	0.7	1.0
N_q	2.5	3.4	4.9

Noise temperature $T_n \leq 600$ mK

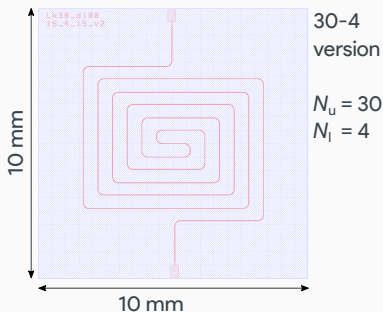
DARTWARS goal accomplished in the first prototype



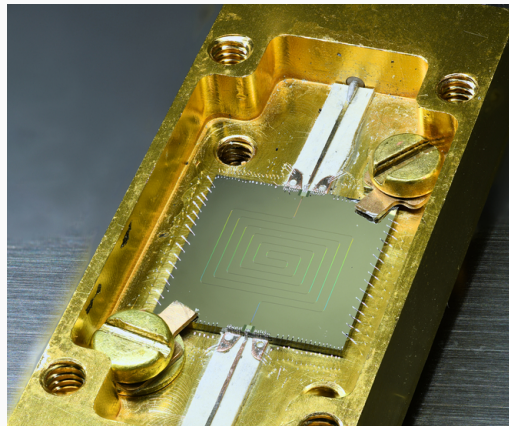
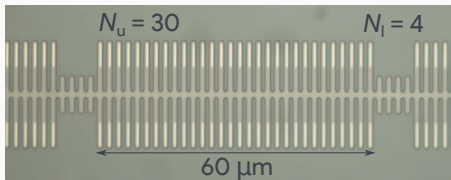
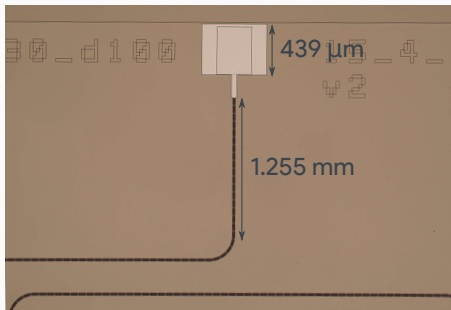
■ Si-substrate
 ■ NbTiN
 ■ Copper Box
 ■ Amorphous silicon



- NbTiN line with higher kinetic inductance $L_k = 30$ pH/sq (instead of 10 pH/sq) [IEEE Trans. Appl. Supercond. 33,5 \(2023\) 1700905](#);
- Inverted-microstrip lines provide higher capacitance due to the amorphous silicon (a-Si) dielectric;



- Two-arm spiral layout to optimize the chip size;
- Each supercell composed by:
 - $N_u = 30$ unloaded cells and $N_l = 6$ loaded cells;
- Total number of supercells: $N_{sc} = 1200$;
- Total number of cells: $N_c = 40800 \Rightarrow$ Total line length: $L_{tot} \sim 8.2$ cm (for the previous CPW version: $L_{tot} \sim 33$ cm);
- Chip sizes: 1×1 cm² (for the previous CPW version: 2×2 cm²);
- Expected gain: $G > 25$ dB, centered at 6 GHz;
- Expected pump frequency: $f_p \sim 12$ GHz;



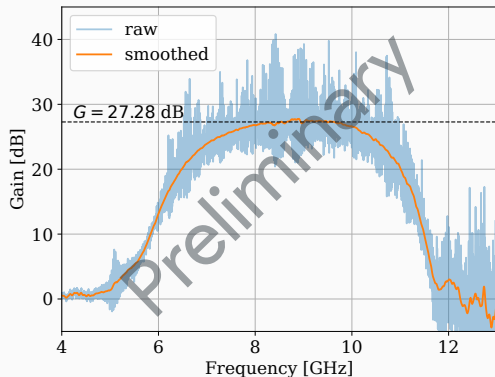
- Version v1 produced in Summer 2024 and published in [J.Low Temp.Phys. 215 \(2024\) 3-4, 152-160](#);
- **Version v2** produced in Fall 2023;

Version v2: 12 prototypes tested:

- 10/12 amplifiers showed a gain $G > 20$ dB;
- Fabrication yield: 83% (2 not working devices)
- $G = (20 - 27)$ dB ✓ 😊;

For the best devices:

NbTiN thickness :	$t = 10$ nm	lower than CPW	✓ 😊
Kinetic Inductance:	$L_0 \sim 30$ pH/sq	higher than CPW	✓ 😊
Critical current:	$I_c \sim 0.8$ mA	lower than CPW	✓ 😊
Scaling current :	$I_* \sim 2.8$ mA	lower than CPW	✓ 😊
Bias current :	$I_{dc} \sim 0.5$ mA	lower than CPW	✓ 😊
Pump power:	$P_p \sim -40$ dBm	lower than CPW	✓ 😊
1 dB compression point:	$P_{1dB} \sim -70$ dBm	compatible CPW	✓ 😊
3 dB bandwidth:	$B = 3.2$ GHz	compatible CPW	✓ 😊

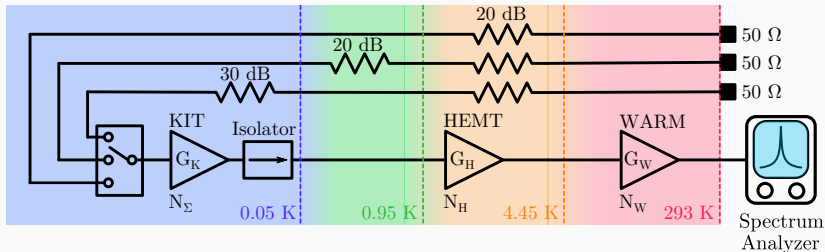


... but ...

- Line impedance lower than expected $Z_0 \sim 40 \Omega$ 😞
- Gain centered at higher frequency: $f_{center} = 8.3$ GHz 😞

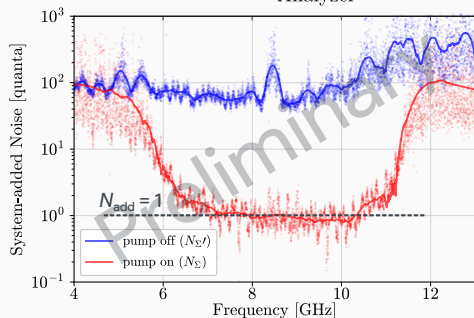
Fabrication issues

- Lower kinetic inductance: $L_k = 25$ pH/sq 😞
- Lower dielectric constant: $\epsilon_r = 8.6$ 😞

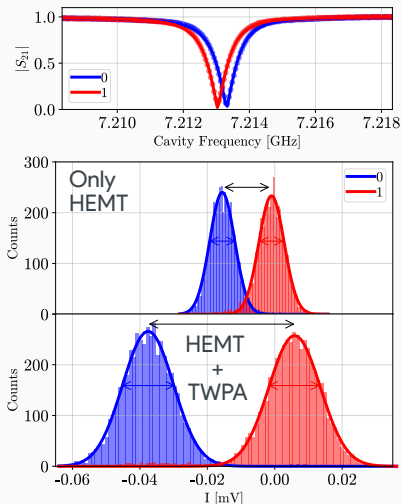


- Modified y-factor (hot/cold) method for measuring the noise;
- Full loss characterization of each component (all at base temperatures);
- KI-TWPA performance creeping up on the SQL $\checkmark \text{😊}$:

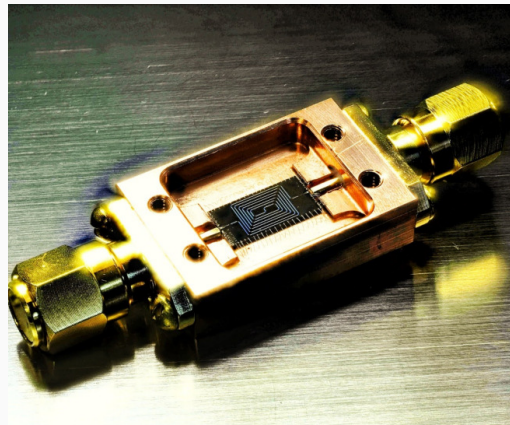
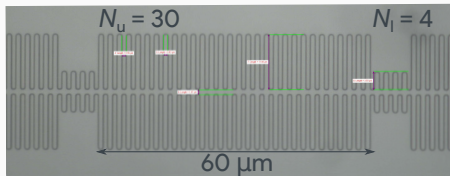
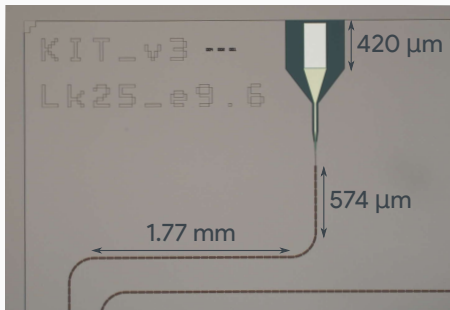
$$N_{\text{add}} \simeq 1 \text{ quanta} \Rightarrow T_N = 400 \text{ mK @ } 8 \text{ GHz}$$
- Equivalent results with a shot-noise tunnel junction (SNTJ) source;



- Readout of an 8-qubit array with **cavities** in the range from **5.8 to 7.2 GHz**;
- TWPA gain centered at **8.2 GHz** \Rightarrow cavities fall in the lower cutoff;
- Pump tone properly filtered to minimize any leakage in the qubit array;
- Only **10-15 dB** of on-off gain is available in that region (probably less considering a line loss of around 3 dB);
- Inside the bandwidth maximum improvement in the state measurement **SNR by a factor of 1.45**, and increase the **fidelity from 96.2% to 97.8%**;
- Encouraging results despite the mismatch between TWPA bandwidth and qubit frequencies;
- A new qubit array optimized for fast readout and a new TWPA will be used to perform better measurements;



IEEE Trans. Appl. Supercond. 35 (2025) 5, 1500305



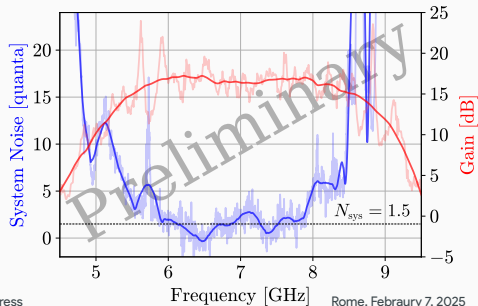
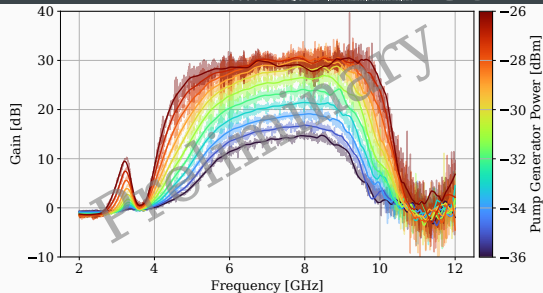
Version v3 produced in Summer 2024

Paper ready to be submitted on PRX Quantum

- **Optimized stub lengths** for covering different kinetic inductance L_k and permittivity ϵ_r combinations;
- **Optimized transitions** from stub-loaded microstrip to standard microstrip to CPW ports;
- **Optimized copper box with spring-loaded pogo pins** to avoid bonds;

Preliminary results

- Tunable gain up to $G = 30$ dB;
- Very low gain ripple $r < 1.5$ dB_{rms} over 3 GHz of bandwidth;
- Transmission line with characteristic impedance around $Z_0 = 49 \Omega$ (that reach 50 Ω by applying the bias);
- System noise around $N_{\text{sys}} = 1.5$ (measurement with improved configuration in progress);



- For Italian Developments:
 - Transition from a stub-loaded CPW line to an inverted microstrip line, following the NIST solution;
 - Design of test structures for extracting the dielectric and superconducting characteristic parameters;
 - Design and production of the first inverted microstrip TWPA amplifier before June (Q2);
- For the Development in Collaboration with NIST:
 - Versions v2 and v3 of the amplifier have shown highly competitive performance in terms of gain, ripple, and noise;
 - Version v2 has been successfully used for qubit array readout;
 - Version v3 currently under characterization and optimization;
 - A new qubit array, optimized for fast readout, is in development for readout demonstration with Version V3;
 - Optimization of a new version with on-chip bias tees and directional couplers/diplexers;
 - Optimization of new versions for sub-GHz applications (MKIDs) and high-frequency applications (>20 GHz, hot qubits, and cavities).

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